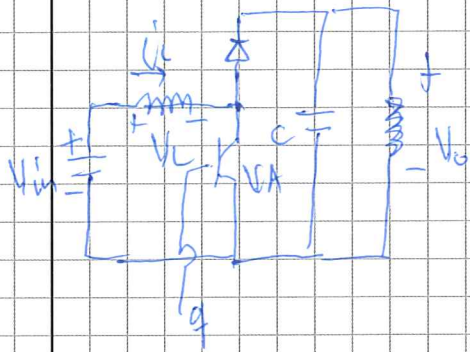




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 Kandidatnr. : 226
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 Ark nr. : 1. av 10

Question 1 DC-DC Boost Converter



$L = 25 \mu H$
 $V_{in} = 12 V$
 $D = \frac{T_{on}}{T_s} = 0,4$
 $f_s = 400 kHz$
 $P_o = 25 W$

$T_s = \frac{1}{f_s} = \frac{1}{400 kHz}$

$T_s = 2,5 \mu s$

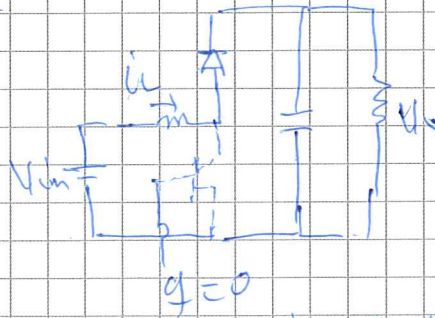
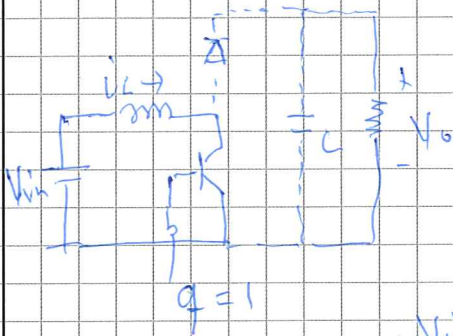
$\frac{V_o}{V_{in}} = \frac{1}{1-D}$

$V_o = \frac{V_{in}}{1-D}$

$V_o = \frac{12}{1-0,4}$
 $= 20 V$

$T_{on} = D T_s = 1 \mu s$

ⓐ



when $q=1$ $V_A = 0$
 $q=0$ $V_A = V_{in}$

when $q=1$ $V_L = V_{in}$

$q=0$ $V_L = -(V_o - V_{in})$
 $= -8 V$

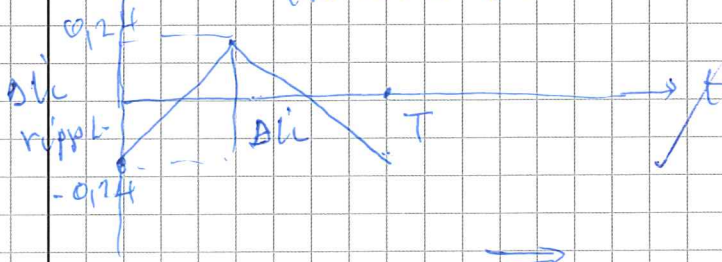
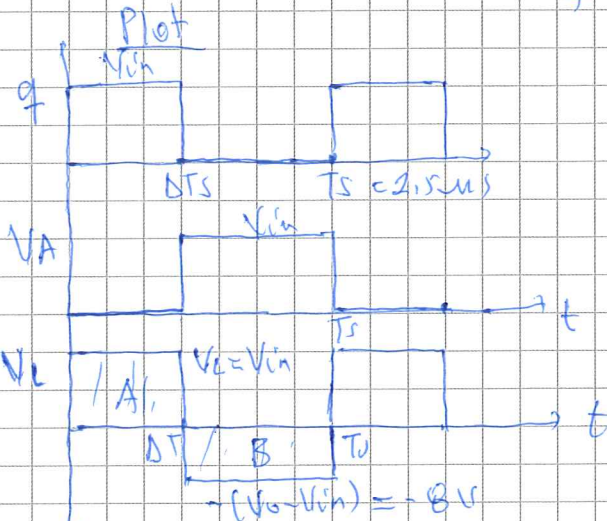
$\Delta V_L = \frac{V_{in} \Delta T}{L}$

$= \frac{12 \cdot 0,4 \cdot 2,5 \times 10^{-6}}{25 \mu H}$

$\Delta V_L = 0,48 A$
 ripple

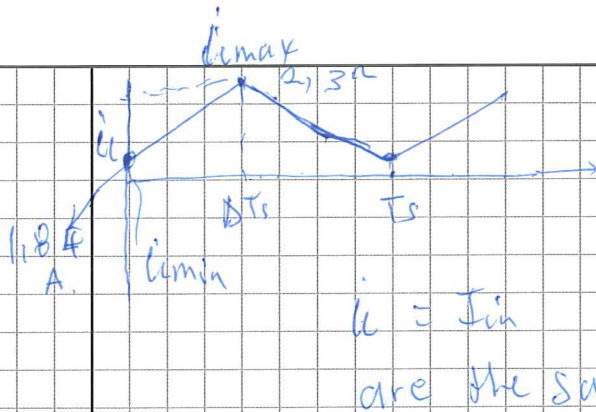
$I_L = I_{in} = \frac{P_{in}}{V_{in}} = \frac{25 W}{12}$

$I_L = I_{in} = 2,08 A$





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$$i_{Lmax} = 2.08 + \frac{\Delta i_L}{2} = 2.32 \text{ A}$$

$$i_{Lmin} = 2.08 - \frac{\Delta i_L}{2} = 1.84 \text{ A}$$

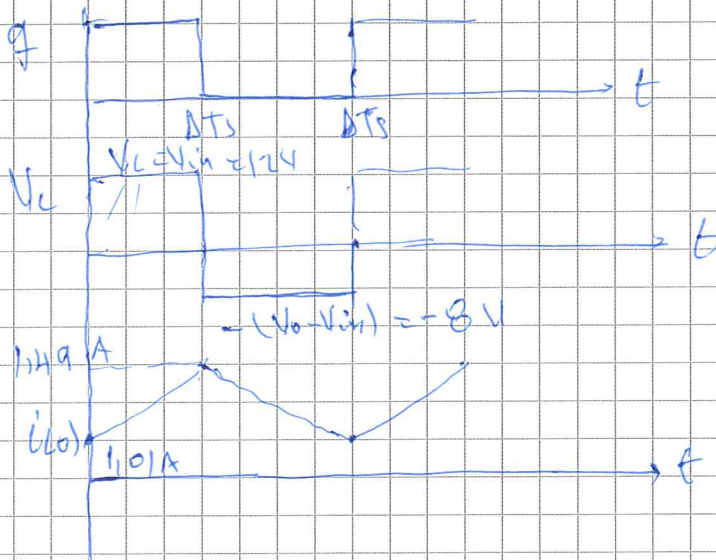
(b) $P_o = 15 \text{ W}$ $i_L = I_{in} = \frac{P_i/P_o}{V_{in}} = \frac{15}{12} = 1.25 \text{ A}$

Δi_L - ripple = 0.48 A
 ↳ unchanged

V_{in} - is unchanged

$$\Delta i_L \text{ ripple} = \frac{V_{in} \Delta T_s}{L} = \frac{12 \text{ V} \cdot 0.4 \cdot 2.5 \mu\text{s}}{25 \text{ mH}} = 0.48$$

Plot



$$q = 1 \quad V_c = V_{in} = 12 \text{ V}$$

$$q = 0 \quad V_c = -(V_o - V_{in}) = -8 \text{ V}$$

$$i_{Lmax} = 1.25 + \frac{\Delta i_L}{2} = 1.49 \text{ A}$$

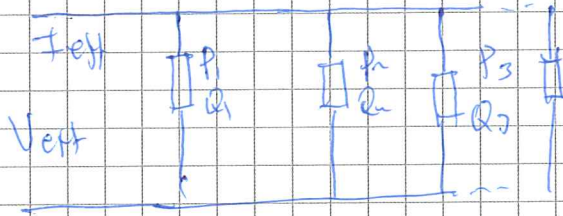
$$i_{Lmin} = 1.25 - \frac{\Delta i_L}{2} = 1.01 \text{ A}$$





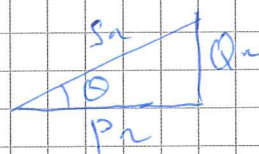
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 Kandidatnr. : 226
 Dato : 23.05.2017
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Question 2



$P_1 = 10 \text{ kW}$ $pf_1 = 1$
 $Q_1 = 0$

$P_2 = 20 \text{ kW}$ $pf_2 = 0,5$ lagging

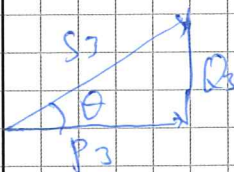


$\cos^{-1} 0,5 = \theta = 60^\circ$

$\tan \theta = \frac{Q_2}{P_2}$

$Q_2 = \tan 60 \cdot 20 \text{ kW}$
 $= 34,64 \text{ kVAR}$

$P_3 = 15 \text{ kW}$, $pf_3 = 0,6$ lag



$\cos^{-1} 0,6 = \theta = 53,13^\circ$

$\tan \theta = \frac{Q_3}{P_3}$

$Q_3 = \tan 53,13 \cdot 15 \text{ kW} = 20 \text{ kVAR}$

So $P_T = P_1 + P_2 + P_3 = 10 \text{ kW} + 20 \text{ kW} + 15 \text{ kW} = 45 \text{ kW}$

$Q_T = Q_1 + Q_2 + Q_3 = 0 + 34,64 \text{ kVAR} + 20 \text{ kVAR} = 54,64 \text{ kVAR}$



$ST = \sqrt{P_T^2 + Q_T^2}$
 $= 70,785 \text{ kVA}$

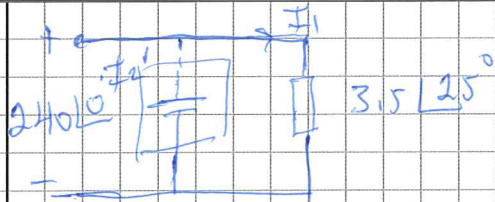
$PF_T = \cos \phi = \frac{P_T}{S_T} = 0,6357$

$S_T = V_{eff} I_{eff}$

$I_{eff} = \frac{S_T}{V_{eff}} = \frac{70,785 \text{ kVA}}{6 \text{ kV}} = 11,798 \text{ A}$ ($\cos^{-1} 0,6357$)



(b)



$$Z = 3,5 \angle 25^\circ$$

$$P_{f1} = \cos 25 = 0,906 \text{ laggin}$$

$$P_{\text{improva}} = 0,95 \text{ laggin}$$

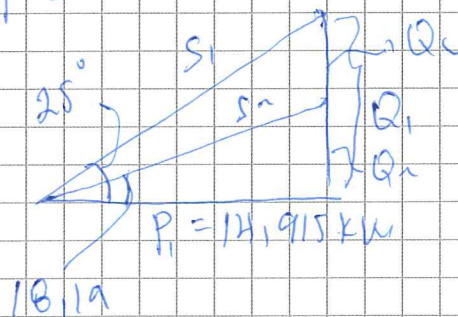
I_1 - Before capacitor is connected will be -

$$I_1 = \frac{240 \angle 0^\circ}{3,5 \angle 25^\circ} = 68,57 \angle -25^\circ$$

- Active power is always the same:

$$P = V \cdot I \cos \phi = 240 \cdot 68,57 \cos(-25) = 14,915 \text{ kW}$$

$P =$



$$\tan 25 = \frac{Q_1}{P}$$

$$Q_1 = \tan 25 \cdot 14,915 \text{ kW} = 6,955 \text{ kVAR}$$

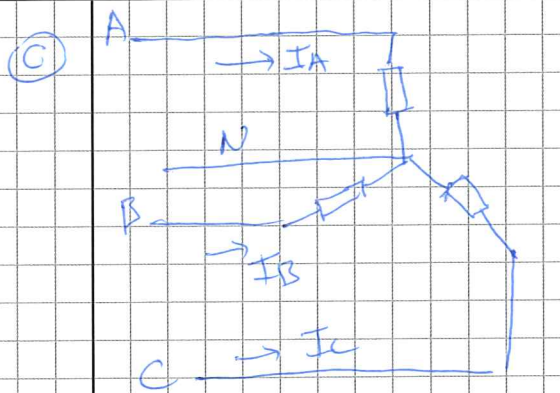
$$Q_2 = \tan 18,19 \cdot 14,915 \text{ kW} = 4,901 \text{ kVAR}$$

$$Q_c = Q_1 - Q_2$$

$$= 6,955 \text{ kVAR} - 4,901 \text{ kVAR}$$

$$= 2,054 \text{ kVar}$$

~~$\Rightarrow 205,4 \text{ VAR}$ must be provided~~



$$V_{L-L} = 169,7 \text{ V}$$

$$V_{\text{phase}} = \frac{169,7}{\sqrt{3}} = 97,98 \text{ V}$$

Y-connected line current is the same as phase current

$$Z = 20 \angle -30^\circ$$

$$I_A = \frac{97,98 \angle -90}{20 \angle -30} = 4,899 \angle -60$$

$$I_B = \frac{97,98 \angle 30}{20 \angle -30} = 4,899 \angle 60$$

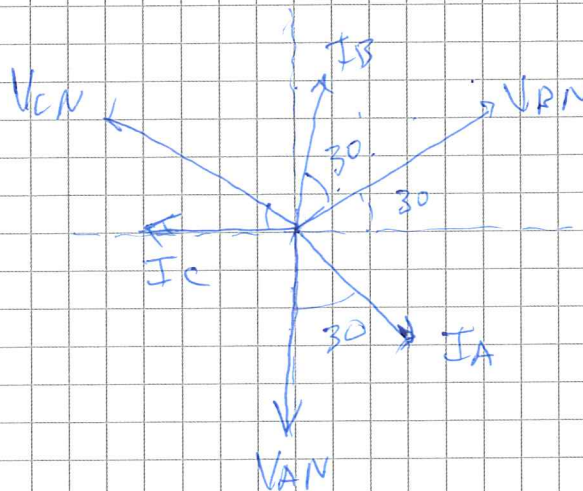
$$I_C = \frac{97,98 \angle 150}{20 \angle -30} = 4,899 \angle 180$$

$$V_{AN} = 97,98 \angle -90$$

$$V_{BN} = 97,98 \angle 30$$

$$V_{CN} = 97,98 \angle 150$$

Phasor-Diagram





Question 3

① Bus admittance matrix Y_{bus} is formed by considering KCL in the nodes of transmission line buses.

$$\text{i.e. } I_k = \sum_{k=1}^n Y_k V_k \quad (k=1, 2, \dots, n)$$

n - is number of nodes

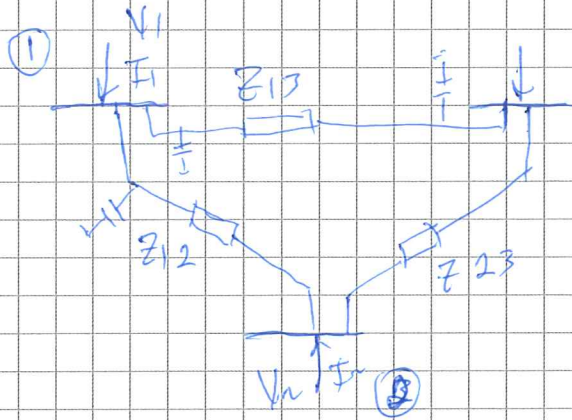
$$\begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ \vdots \\ I_n \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} & Y_{14} & \dots & Y_{1n} \\ Y_{21} & Y_{22} & Y_{23} & Y_{24} & \dots & Y_{2n} \\ Y_{31} & Y_{32} & Y_{33} & Y_{34} & \dots & Y_{3n} \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ Y_{n1} & Y_{n2} & Y_{n3} & Y_{n4} & \dots & Y_{nn} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ \vdots \\ V_n \end{bmatrix}$$

$$I_{bus} = Y_{bus} V_{bus}$$

Admittance matrix Y_{bus} is preferred in comparison to the bus impedance matrix Z_{bus} b/c normally buses are connected to one or two other buses, so when we deal with admittance matrix in the load flow studies it is simple and sparse where ~~the~~ some parts goes to zero, where as Z_{bus} is huge and can complicate the analysis.



(b)



(3)

$V = 345 \text{ kV}$
 $Z_{12} = 5,55 + j56,4 \Omega$
 $Z_{13} = 7,40 + j75,2 \Omega$
 $Z_{23} = 5,55 + j56,4 \Omega$

$Z_{12} \text{ pu} = \frac{(5,55 + j56,4) 100 \text{ MVA}}{(345 \text{ k})^2} = 0,0047 + j0,0474 \text{ pu}$

$Z_{13} = \frac{(7,40 + j75,2) 100 \text{ MVA}}{(345 \text{ k})^2} = 0,0062 + j0,0632 \text{ pu}$

$Z_{23} = Z_{12} = 0,0047 + j0,0474 \text{ pu}$

$$\begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} \\ Y_{21} & Y_{22} & Y_{23} \\ Y_{31} & Y_{32} & Y_{33} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \end{bmatrix}$$

$Y_{11} = \frac{1}{Z_{12}} + \frac{1}{Z_{13}} = 3,61 - j36,56$

$Y_{12} = -\frac{1}{Z_{12}} = -2,07 + j20,89$

$Y_{13} = -\frac{1}{Z_{13}} = -1,54 + j15,67$

$Y_{21} = -\frac{1}{Z_{12}} = -2,07 + j20,89$

$Y_{31} = -\frac{1}{Z_{13}} = -1,54 + j15,67$

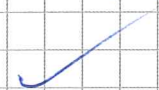
$Y_{22} = \frac{1}{Z_{12}} + \frac{1}{Z_{23}} = 4,14 - j41,78$

$Y_{32} = \frac{1}{Z_{23}} = -2,07 + j20,89$

$Y_{23} = -\frac{1}{Z_{23}} = -2,07 + j20,89$

$Y_{33} = \frac{1}{Z_{13}} + \frac{1}{Z_{23}} = 3,61 - j36,56$

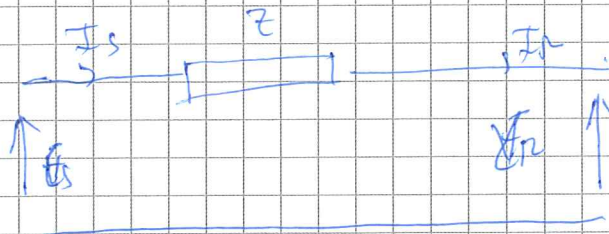
$$\begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix} = \begin{bmatrix} 3,61 - j36,56 & -2,07 + j20,89 & -1,54 + j15,67 \\ -2,07 + j20,89 & 4,14 - j41,78 & -2,07 + j20,89 \\ -1,54 + j15,67 & -2,07 + j20,89 & 3,61 - j36,56 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \end{bmatrix}$$





Question
#

(a) 3φ, 50Hz, load = 15 MW



$V_r = 10 \text{ kV}$
 $\text{pf} = 0,8 \text{ laggin}$
 $\phi_r = \cos^{-1} 0,8 = 36,87^\circ$

$$E_s = E_r + I R \cos \phi_r + I X \sin \phi_r$$

$$Z = (0,102 + j0,65) 20 = 0,4 + j13$$

$$P_{\text{phase}} = \frac{15 \text{ MW}}{3} = 5 \text{ MW}$$

$$P = V_r I_r \cos \phi \Rightarrow I_r = I = \frac{5 \text{ MW}}{10 \text{ k} \cdot 0,8} = 625 \frac{\text{A}}{\cos \phi}$$

$$E_s = 10 \text{ k} \angle 0^\circ + 625 (0,4 \cdot 0,8 + j13 \cdot 0,6)$$

$$\approx 10 \text{ k} \angle 0^\circ + 200 + j4,875$$

$$\approx 10,2 + j4,875$$

$$E_s = 11,305 \text{ k} \angle 25,15^\circ$$

Voltage regulation

$$E_{r \text{ no load}} = E_r$$

$$V_r = \frac{E_{r \text{ no load}} - E_{\text{full load}}}{E_{\text{full load}}}$$

$$V_r \% = \frac{11,307 - 10}{10} 100\%$$

$$= 13,07\%$$



(c) 3 ϕ , 3-wire $V_{LL} = 250\text{ V}$

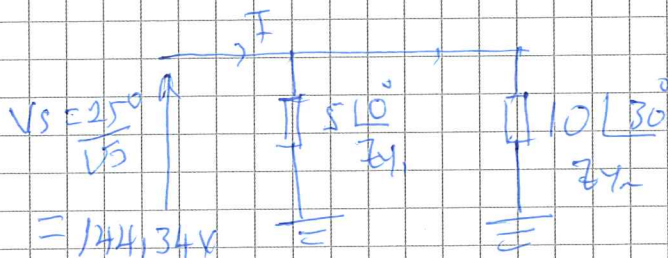
$$Z_{\Delta} = 15 \angle 0^{\circ}$$

$$Z_{\Delta} = 10 \angle 30^{\circ}$$

Convert the Δ -load to Y-load

$$Z_Y = \frac{Z_{\Delta}}{3} = \frac{15 \angle 0^{\circ}}{3} = 5 \angle 0^{\circ}$$

By using single-line equivalent ckt



$$= 144,34\text{ V}$$

$$Z_T = \frac{Z_{Y1} \cdot Z_{Y2}}{Z_{Y1} + Z_{Y2}}$$

$$= \frac{5 \angle 0^{\circ} \cdot 10 \angle 30^{\circ}}{5 \angle 0^{\circ} + 10 \angle 30^{\circ}}$$

$$Z_T = \frac{50 \angle 30^{\circ}}{13,66 + j5} = \frac{50 \angle 30^{\circ}}{14,55 \angle 20,1^{\circ}}$$

$$= 3,44 \angle 9,9^{\circ}$$

So, combined pf = $\cos 9,9^{\circ} = \underline{\underline{0,985}}$

Active $3\text{ V I} \cos \phi$

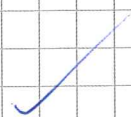
$$I = \frac{V_{LL}}{Z} = \frac{144,34 \angle 0^{\circ}}{3,44 \angle 9,9^{\circ}}$$

$$P_{\text{active}} = 144,34 \cdot 41,96 \cdot 0,985 \times 3$$

$$= 41,96 \angle 9,9^{\circ}$$

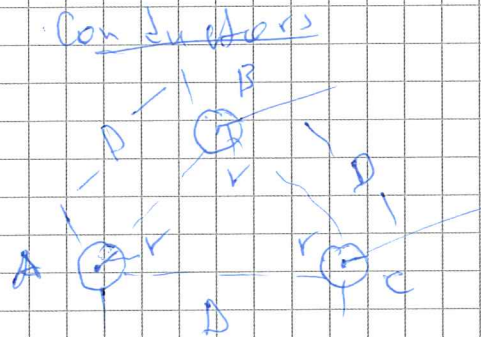
$$= 17896,67\text{ W}$$

$$\approx \underline{\underline{17,897 \text{ kW}}}$$





①



Balanced condition
 $I_a + I_b + I_c = 0$

If we take for the flux linkage of conductor (A)

$$\lambda_a = \frac{\mu_0}{2\pi} I_a \ln \frac{1}{r} + \frac{\mu_0}{2\pi} I_b \ln \frac{1}{D} + \frac{\mu_0}{2\pi} I_c \ln \frac{1}{D}$$

λ_a - linkage due to the three conductors

$$\lambda_a = \frac{\mu_0}{2\pi} I_a \ln \frac{1}{r} + (I_b + I_c) \frac{\mu_0}{2\pi} \ln \frac{1}{D}$$

$$I_a + I_b + I_c = 0$$

$$I_b + I_c = -I_a$$

$$\lambda_a = \frac{\mu_0}{2\pi} I_a \ln \frac{1}{r} - \frac{\mu_0}{2\pi} I_a \ln \frac{1}{D} \rightarrow$$

$$\lambda_a = \frac{\mu_0}{2\pi} I_a \left(\ln \frac{1}{r} - \ln \frac{1}{D} \right) = \ln \frac{D}{r}$$

$$\lambda_a = \frac{\mu_0}{2\pi} I_a \ln \frac{D}{r}$$

$$\text{Inductance } L = \frac{\lambda_a}{I_a} = \frac{\mu_0}{2\pi} \ln \frac{D}{r}$$

So Inductance

$$L = \frac{\mu_0}{2\pi} \ln \frac{D}{r}$$